

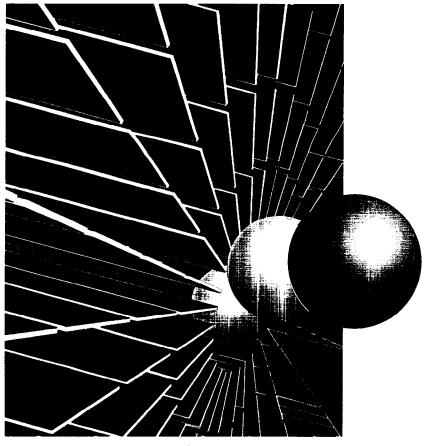


Research, Development and Technology

RDT 02-01

Water Reducing Admixtures in Portland Cement Concrete Pavement (PCCP) on Route 60, Carter County

RI 00-001(B)



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16. Abstract				
The purpose of this investigation was to verify	and supplement the fi	ndings of research in	vestigation RI00-001A, "Water Reducing	
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savings of adding a Type A water reducer and				
	6			
This research report presents the testing result	s from a second field st	udy conducted on Re	oute 60 in Carter County (J9P0282) in	
which a PCCP mix containing a Type A water				
PCCP mix. The concrete specimens fabricate				
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28-day compressive strength (AASI				
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RESEARCH INVESTIGATION RI00-001B

FIELD STUDY WATER REDUCING ADMIXTURES IN PCCP ON RT 60, CARTER COUNTY

PREPARED BY
MISSOURI DEPARTMENT OF TRANSPORTATION
RESEARCH, DEVELOPMENT, AND TECHNOLOGY

Written by:

JASON M. BLOMBERG, E.I.T. Senior Research and Development Assistant

> JEFFERSON CITY, MISSOURI Date Submitted: January 22, 2002

The opinions, findings and conclusions expressed in this publication are those of the principal investigator and the Research, Development, and Technology Division of the Missouri Department of Transportation.

They are not necessarily those of the U.S. Department of Transportation, Federal Highway Administration. This report does not constitute a standard, specification or regulation.

:			

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Andrew Horstman, Lola Eudaley, and Debra Krueger, MoDOT-District 9 Construction, contacts for project information.

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Eric Burks, Larry Diaz, Chris Graham, and Dave Amos, RD&T technicians, conducted field sampling and fabricating concrete specimens for this project.

Steve Jackson, Physical Testing Supervisor, scheduled and tested all concrete specimens fabricated in this project and reported the results in a timely manner.

The author is also grateful to John Donahue for manuscript review.

EXECUTIVE SUMMARY

This study was conducted to verify and supplement the findings of research investigation RI00-001A, "Water Reducing Admixtures in PCCP Mixes", Report No. RDT 01-004. The objective of RI00-001 is to determine the potential benefits and cost savings of adding a Type A water reducer and lowering the cement content in MoDOT's PCCP mixes. The previous field study indicated poor freeze/thaw performance by both the control and water reducer (WR) mixes, which was thought to be the characteristics of the aggregate source. Also, the control mix had approximately 12% higher freeze/thaw durability compared to the WR mix. The results from the previous study initiated this field study to verify the performance characteristics of the WR mix, especially the freeze/thaw durability.

This report presents the testing results from the second field study conducted on Route 60 in Carter County (J9P0282) in which a PCCP mix containing a Type A water reducer with a ¼-sack reduction in cement content was compared to MoDOT's conventional PCCP mix. The main findings of this study are summarized as follows:

- > Both the control and the WR mixes had a freeze/thaw durability of 82%. The water reducer shows no additional benefit or detriment to the freeze/thaw durability of concrete in this study.
- > The air void systems for the control and water reducer mixes were satisfactory for good freeze/thaw resistance.
- > The WR mix significantly reduced chloride permeability compared to the control mix.
- > The WR mix was significantly higher in compressive and flexural strengths compared to the control mix.
- > The PCCP mix containing the water reducer with a ¼-sack reduction in cement cost less than a standard PCCP mix. The proposed savings for this study was approximately \$0.59 per cubic yard.

Based upon the previous laboratory and field study and the results obtained in this investigation, Research, Development, and Technology conclude that Type A water reducers with a ¼-sack reduction in cement can be used to obtain better concrete characteristics at lower costs compared to conventional PCCP mixes. Research, Development, and Technology recommend that revisions be made to allow Type A water reducer with ¼-sack cement reductions in MoDOT PCCP mix designs. Further investigation of Type A water reducers and pozzolans (i.e. slag, flyash, silica fume) are currently underway in the laboratory and final conclusions should be available in 2003.

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OBJECTIVE

The objective of this project is to verify and supplement the findings of research investigation RI00-001(A), "Water Reducing Admixtures in PCCP Mixes." The objective of RI00-001 is to determine the potential benefits and cost savings of adding a Type A water reducer and lowering the cement content in MoDOT's PCCP mixes.

Concrete specimens were fabricated from a project on Rt. 60 in Carter Co. and were tested to determine the following fresh and hardened characteristics of the PCCP mixes:

w/c ratio	
slump	(AASHTO T119)
air content	(AASHTO T152)
freeze-thaw durability	(AASHTO T161)
air void analysis	(ASTM C457)
rapid chloride permeability	(AASHTO T277)
7-day compressive strength	(AASHTO T22)
28-day compressive strength	(AASHTO T22)
7-day flexural strength	(AASHTO T97 or T177)
28-day flexural strength	(AASHTO T97 or T177)

TECHNICAL APPROACH

Concrete field-testing was conducted on a PCCP project on Route 60 in Carter County (J9P0282). PCCP mixes containing a Type A water reducer with ¼-sack cement reduction ("WR mixes") were compared to MoDOT's standard PCCP mixes without water reducer and cement reductions ("control mixes") to determine the potential benefits and cost savings of a Type A water reducer.

Concrete specimens were fabricated from the control and WR mixes and laboratory tested for freeze thaw durability, air void structure, chloride permeability, and compressive and flexural strengths, following the appropriate AASHTO and ASTM Standard Specifications as listed above. The fabrication of concrete test specimens was conducted according to AASHTO T23, Making and Curing Concrete Test Specimens in the Field.

For a thorough comparison of water reducer mixes versus the control mixes, the contractor was requested to follow a certain paving sequence. The paving sequence started with a control mix, then switched to the WR mix, and finally returned back to the control mix, all within the same day. Sampling and fabricating of the concrete test specimens were performed at four intervals within this sequence. Figure 1 illustrates the order of the paving sequence. Sampling of concrete was conducted at the batch plant where a representative sample was obtained for each sampling interval. Each test interval within the paving sequence represents approximately 130 cubic yards of concrete in which sampling and fabrication of test specimens were conducted. Specimens fabricated from Control Interval 1 (CI-1) represented the sampling of the first control mix. The

Water Reducer Intervals 1 and 2 (WRI-1&2) represented the water reducer mix with a ¼ - sack reduction in cement per cubic yard. CI-2 completed the sampling for the control mix. The same paving sequence of four intervals was then repeated a second day during which concrete specimens were fabricated and tested from CI-3, followed by WRI-3 & 4, and finally CI-4.

Prior to the actual paving, the contractor was required to submit the proposed mix designs which included material sources and the water cement ratios, provide an outline of the proposed savings comparing the cost of the additional admixture to the savings in cement, and provide specific construction details to insure uniformity in materials, mix designs, and placement procedures.

The source/manufacturer and description of the materials that were used for the field study are as follows:

Coarse Aggregate: Gasconade Dolomite, Williamsville Stone #4

Gradation B

Fine Aggregate: Crowley Ridge Class A

Brown's Sand and Gravel

Dexter, MO

Cement: LoneStar

Cape Girardeau Plant

Type 1

Air Agent: General Resource Technology (GRT)

Polychem VR

Air Entraining Admixture

Water Reducer: General Resource Technology (GRT)

(Used in WR mixes only) Polychem 400NC

Type A Water Reducer

RESULTS AND DISCUSSION

Concrete Characteristics

The results from field testing of the water reducer mixes and control mixes for freeze thaw durability, air void structure, chloride permeability, and compressive and flexural strengths of each study are described within the following sections. Fresh concrete characteristics (slump, air, w/c ratio) are listed in the Table 1. Control Interval 1 (CI-1) had only 1.5 % air content, which is well below the Missouri Standard Specifications for Highway Construction (4 - 7 %). Therefore, the results from this interval are not included in the analysis. Water Reducer Interval 1 (WRI-1) contained 8 % air content, which also did not meet air entrainment requirements by specification. However, the results were considered reasonable to include in the final analysis.

Freeze/Thaw Durability (AASHTO T161)

Concrete beams were fabricated on the Rt. 60 project and tested according to AASHTO T161, Resistance of Concrete to Rapid Freezing and Thawing. Six or eight beam specimens were fabricated from each interval and tested in 300 freeze/thaw cycles. The freeze/thaw durability were calculated and averaged for each interval and are listed in Table 2. Freeze/Thaw durability for individual test specimens can be found in Appendix A.

The freeze/thaw (F/T) durability of both the control mix and the water reducer mix averaged 82%. The F/T testing results indicate that the water reducer had no benefit or detriment to the freeze/thaw durability of concrete in this study.

The F/T results from CI-1 were not included in this study. The mix from CI-1 contained only 1.5% air content, which does not meet MoDOT specifications and is not acceptable for good freeze/thaw performance. The average F/T durability of CI-1 was 44%.

WRI-1 exceeded MoDOT specification for air content by 1%. The increased air content did not affect the freeze/thaw durability. The average F/T durability of WRI-1 was 82%. Two specimens from WRI-3 were discarded and not included in the average. The two specimens were significantly lower than the other six specimens within the same interval. The reason for this difference is unclear, but may be due to segregation or poor consolidation of the test specimens.

Air Void Analysis

Eight specimens (one from each interval) were fabricated at the Rt. 60 project in which the air void structures were analyzed and compared. The laboratory worksheets are included in Appendix B. The water reducer in this field study did not significantly affect the air void structure compared to the control mix. However, the WR mix appeared to have slightly larger sized air bubbles that were spaced further apart compared to the control mix. The WR mix met all American Concrete Institute (ACI) recommended air void parameters. The control mix's specific surface was slightly higher than what is recommended by ACI. It appears that both the WR and control mixes had acceptable air void structure for good freeze/thaw durability as was indicated by the F/T results.

Rapid Chloride Permeability (AASHTO T 277)

The WR mixes in this study had significantly lower chloride permeability compared to the control mix. The average permeability (Coulombs) of the WR mix and the control mix are listed in Table 3.

Generally, permeability greater than 4000 C is considered high. Moderate permeability is considered between the ranges 2000 – 4000 C. The water reducer appeared to decrease the permeability of a standard mix from a high permeability range to the moderate range.

Compressive Strength (AASHTO T22) and Flexural Strength (AASHTO T97)

Compressive and flexural strength data were collected from 7 and 28-day concrete cylinders and beams taken from both the control mix and the water reducer mix. The average 7 and 28-day strengths for both mixes are listed in Table 4. Figures 2 and 3 graphically show each water reducer interval compared to the control for compressive and flexural strengths, respectively. Appendix D contains strength results for individual specimens taken from each interval and other mix characteristics. Both the water reducer mix and the control mix had similar water/cement ratios (approximately 0.45).

The strength results from CI-1 were not included in this study. The mix from CI-1 contained only 1.5 % air content. This caused higher than normal strengths and would only skew the average results.

WRI-1 exceeded MoDOT specification for air content by 1%. Although it did not meet MoDOT specifications, it was included into calculating the average. This was the only water-reducing interval that had lower strengths compared to the control mixes due to the 1% higher air content. The higher air content will lead to lower compressive strengths for the interval. Generally for every 1% increase in air content, there is approximately a 10 % reduction in compressive strength².

Effects to Air Entrainment Dosage

Like the previous study has indicated, the air entrainment dosage in this study decreased by over 60%. The control mix required approximately 8 to 9 oz./yd³ and the WR mix required about 3 oz./yd³. Air entrainment dosages vary somewhat in the field and are generally caused by changes in air temperature. However, the addition of water reducer will decrease the amount of air entrainment dosage needed in the mix.

Effects to Water/Cement Ratio

The water/cement (w/c) ratio at the batch plant varied somewhat from the initial mix design. It was also difficult to obtain the exact batch plant sheet in which specimens were taken in this study. Several batch sheets were obtained from approximately the same time frame as when the specimens were fabricated, and an average w/c ratio was calculated. The average water/cement ratios of the control mix and the WR mix for the two testing dates are listed in Table 5. The w/c ratio of the WR mix and control mix were approximately 0.45.

A minimum of a 5% water reduction is a general requirement of AASHTO M 194 for a Type A water reducer. Typical Type A water reducers reduce the water content by approximately 5% to 10%³. The reduction in cement in the WR mix causes a decrease in workability that counteracts the effect of the water reducer when achieving a target slump. Therefore, the water reducer may not change the water/cement ratio when the cement content is decreased. This has also been verified in the previous studies.

CONCLUSIONS

This report presents results from a second field study conducted on Route 60 in Carter County (J9P0282) in which a PCCP mix containing a Type A water reducer with a ¼-sack reduction in cement content was compared to MoDOT's conventional PCCP mix. The main findings of this study are summarized as follows:

- > Both the control and the WR mixes had a freeze/thaw durability of 82%. The water reducer shows no additional benefit or detriment to the freeze/thaw durability of concrete in this study.
- > The air void systems for the control and water reducer mixes were satisfactory for good freeze/thaw resistance.
- > The WR mix significantly reduced chloride permeability compared to the control mix. This was also indicated in the previous study.
- > The WR mix was significantly higher in compressive and flexural strengths compared to the control, which follows the trends of the previous study.
- > The PCCP mix containing the water reducer with a ¼-sack reduction in cement cost less than a standard PCCP mix. The proposed savings for this study was approximately \$0.59 per cubic yard.

RECOMMENDATIONS

Based upon laboratory and field testing results and observations; Research, Development, and Technology recommends the following:

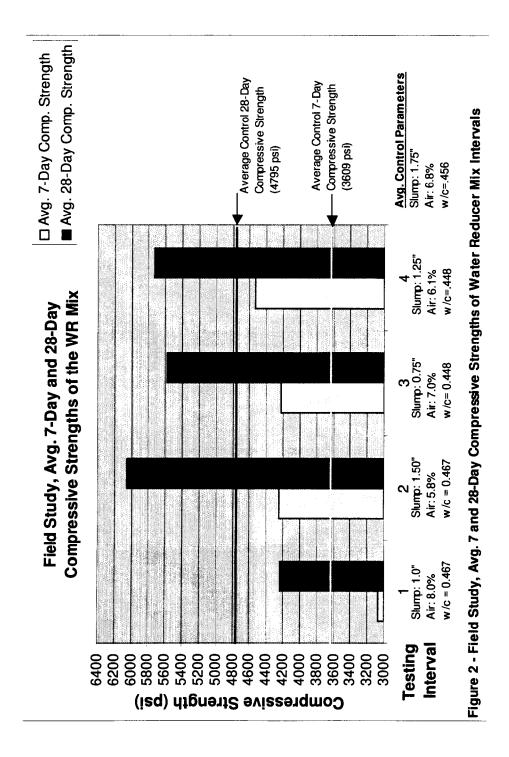
- Research, Development, and Technology recommend that revisions be made to allow Type A water reducer with ¼-sack cement reductions in MoDOT PCCP mix designs.
- > The minimum dosage rate of a Type A water reducer should be established by the dosage rate submitted for the initial admixture approval and within the ranges recommended by the manufacturer.
- > Further evaluation of PCC mixes containing Type A water reducers, cement reductions, and pozzolan replacements is needed to improve PCC performance characteristics, produce a less expensive mix, and become more environmental friendly.

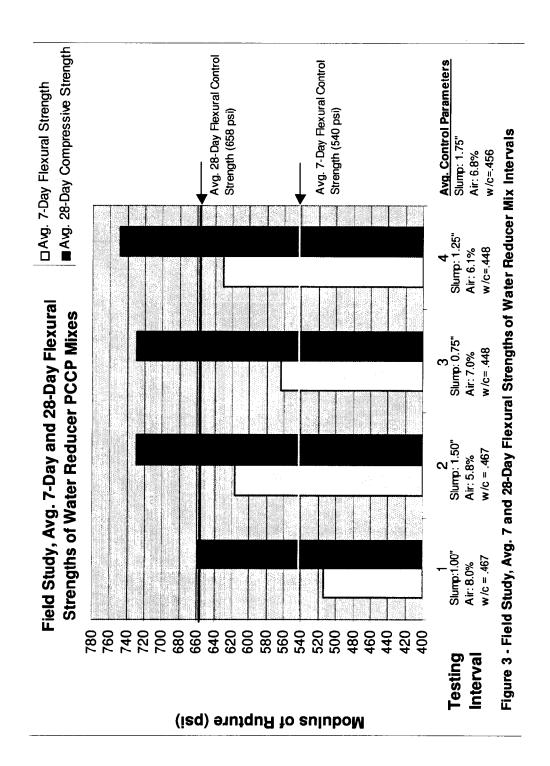
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- 1. 1999 Missouri Standard Specifications for Highway Construction, Section 1054.3. (References AASHTO M194)
- 2. Hover, K.C., *Air Content and Unit Weight of Hardened Concrete*, Significance of Tests and Properties of Concrete and Concrete-Making Materials, ASTM STP 169C, p. 297.
- 3. Portland Cement Association, *Design and Control of Concrete Mixtures*, Thirteenth Edition, Skokie, Illinois, 1994, p. 65 and 66.

ox. 130 yd ³	rol val 2	ox. 130 vd ³	14 4	
represents appr	Control Interval 2	represents appr	Control Interval 4	
/23/01, Each interval	Water Reducer Interval 2	/29/00. Each interval	Water Reducer Interval 4	
ENCE – Poured on 05	Water Reducer Interval 1	JENCE - Poured on 05	Water Reducer Interval 3	
DAY 1 - PAVING SEQUENCE - Poured on 05/23/01, Each interval represents approx. 130 yd ³	Control Interval 1	DAY 2 - PAVING SEOUENCE - Poured on 05/29/00. Each interval represents approx. 130 vd ³	Control Interval 3	

Figure 1 – Field Paving Sequence and Sampling Interval





AVERAGE CONCRETE CHARACTERISTICS						
Interval No.	Cement / Fly Ash (lb/yd³)	Avg. Water Red. (oz./ yd³)	Avg. Air Agent (oz/yd³)	Avg. W/C Ratio	Slump (in)	Air (%)
Control i	573	0	8.0	455	1.5	1.5
Control 2	573	0	8.0	.455	1.5	6.9
Control 3	573	0	9.0	.457	1.75	6.7
Control 4	573	0	9.0	.457	2.25	6.9
AVG	573	0	8.5	.456	1.75	6.8
WR 1	546	20.0	2.5	.467	1.0	8.0
WR 2	546	20.0	2.5	.467	1.5	5.8
WR 3	546	20.0	3.0	.448	.75	7.0
WR 4	546	20.0	3.0	.448	1.25	6.1
AVG	546	20.0	2.8	.458	1.0	6.7

Table 1 – Average Concrete Characteristics

CONTROL INTERVALS	FREEZE/THAW DURABILITY
Control 1	(44) Not Included
Control 2	83.0
Control 3	80.3
Control 4	83.8
Average	82.4
WATER REDUCER	FREEZE/THAW
INTERVALS	DURABILITY
Water Reducer 1	81.6
Water Reducer 2	82.7
Water Reducer 3	80.2
Water Reducer 4	84.1
Average	82.1

Table 2 – Average Freeze/Thaw Durability Results

MIX TYPE	CONTROL MIX	WATER REDUCER MIX
Avg. 28-Day Permeability (C) Top Lift	4941	3481
Avg. 28-Day Permeability (C) Middle Lift	5431	3559
Avg. 56-Day Permeability (C) Bottom Lift	4044	3288

Table 3 – Average Chloride Permeability Results

MIX TYPE	CONTROL MIX	WATER REDUCER MIX
7-Day Compressive Strength (psi)	3609	4021
28-Day Compressive Strength (psi)	4795	5398
7-Day Flexural Strength (psi)	540	581
28-Day Flexural Strength (psi)	658	716

Table 4 - Average Compressive and Flexural Strengths

Control Mix	Avg. w/c Ratio
05/23/01	.455
05/29/01	.452
Water Reducer Mix	Avg. w/c Ratio
05/23/01	.467
05/29/01	.446

Table 5 - Average Water/Cement Ratios

APPENDIX A

(Freeze/Thaw Results)

Mix Name	Cement & FlyAsh (lb/yd^3)	WR (oz/yd^3)	Air Agent (oz/yd^3)	W/C Ratio	Slump (in)	Air (%)	Specimen ID	F/T Durability (%)
Control	<u>573</u>	<u>0.0</u>	<u>8.0</u>	0.412	1.50	1.50	1RJ5B013	27.9
Interval 1							1RJ5B014	38.8
							1RJ5B015	48.0
REEZE/TI	HAW RESUL	TS NOT INC		E TO LOW	AIR CONTE	<u>VT</u>	1RJ5B016	36.9
							1RJ5B017	54.9
				F 15 70 10 10 10 10 10 10 10 10 10 10 10 10 10			1RJ5B018	56.6
							Average	44

Mix Name	Cement & FlyAsh (lb/yd^3)	WR (oz/yd^3)	Air Agent (oz/yd^3)	W/C Ratio	Slump (in)	Air (%)	Specimen ID	F/T Durability (%)
Control	580	0.0	8.0	0.457	1.50	6.90	1RJ5B079	71.6
Interval 2					The second section of the second seco		1RJ5B080	87.7
							1RJ5B081	79.5
	elikaten erekeren erekeren (j. 17. sun 1705 - 170				or a promote the second of the	er territoria de la compa a compa de	1RJ5B082	88.5
Access to the control of the control	to the contract contract contract condition () and () such	mijerovomani navar r svoruprovo ko. r	the automatic consection about a transport and an experimental and distribution	otatatalikudokonostokon, ke mer ee ee ee ee e	e de considére des resources annouvers mes expert e et experience que	all and a control of the second lines of the s	1RJ5B083	84.8
							1RJ5B084	86.1
							Average	83.0

Mix Name	Cement & FlyAsh (lb/yd^3)	WR (oz/yd^3)	Air Agent (oz/yd^3)	W/C Ratio	Slump (in)	Air (%)	Specimen ID	F/T Durability (%)
Control	<u>573</u>	<u>0.0</u>	<u>8.0</u>	<u>0.412</u>	1.75	6.70	1RJ5B101	79.9
Interval 3		and a contract of the contract		111000 1111 1011-1000-1-4040	erroet to treated in the day of the Salahatan annual gaps	throughout princip we consider a consideration of	1RJ5B102	72.2
				THE STREET STREET, STR		edecentroscor - et ac trist acier is conc. (4) (44) ()	1RJ5B103	82.2
41.11	I debt detection and a committee only a symplety of the 1970.	od i danon on one roma cristi actorgiste que certigi	PORTRE CONTROL	the course had the statement on a second or an	mene ner ner met mjestjorn og desett og detek og ekstern norske konstruktion		1RJ5B104	85.0
	i Status Bed annu angunnong unnon sa angung sutur s	p approximately is approximately approximately properly of colors of	there is a second of the secon	Salah'i dan munukun 6. seor susususungg		standarde for a secondary continuation for about	1RJ5B105	74.0
	Badevine out is a sept mapping out of the party	CONTRACTOR AND	descentile literature			Colon II and Control of the state of the sta	1RJ5B106	83.2
		egeneral and a second s	·		- Company Control of C		1RJ5B107 1RJ5B108	86.0 80.1
							Average	80.3

Mix Name	Cement & FlyAsh (lb/yd^3)	WR (oz/yd^3)	Air Agent (oz/yd^3)	W/C Ratio	Slump (in)	Air (%)	Specimen ID	F/T Durability (%)
Control	570	0.0	9.0	0.453	2.25	6.90	1RJ5B173	89.2
Interval 4						attailla dantaman ee matam ee) 11 Gas 100000	1RJ5B174	88.6
					00000107000000	t di Bittiti i i i i i i i i i i i i i i i	1RJ5B175	74.6
					The second secon		1RJ5B176	84.9
							1RJ5B177	74.5
of the second se							1RJ5B178	83.1
P*	the entert of a heaters to like a considerable will		tradistrict and other translations to a section of security and the security of the security o	ess - c-seestin soos tides on tid	entriblische Satie tausanus, visuausevastaas seus us suuri suote	- 25 PME in the net to include the decimal included data	1RJ5B179	88.5
							1RJ5B180	86.9
							Average	83.8

Mix Name Water Reducer Interval 1	Cement & FlyAsh (lb/yd^3) <u>546</u>	WR (oz/yd^3) <i>20.0</i>	Air Agent (oz/yd^3) <u>2.5</u>	W/C Ratio <u>0.428</u>	Slump (in) 1.00	Air (%) 8.00	Specimen ID 1RJ5B035 1RJ5B036 1RJ5B037 1RJ5B038 1RJ5B039 1RJ5B040	F/T Durability (%) 75.9 78.3 85.2 84.7 85.9 79.3
			·				Average	81.6

Mix Name	Cement & FlyAsh (lb/yd^3)	WR (oz/yd^3)	Air Agent (oz/yd^3)	W/C Ratio	Slump (in)	Air (%)	Specimen ID	F/T Durability (%)
Water	544	19.8	2.4	0.368	1.50	5.80	1RJ5B057	80.1
Reducer							1RJ5B058	85.5
Interval 2							1RJ5B059	85.9
							1RJ5B060	80.8
		enter the second				*** ** ***	1RJ5B061	80.3
								83.5
							Average	82.7

Mix Name	Cement & FlyAsh (lb/yd^3)	WR (oz/yd^3)	Air Agent (oz/yd^3)	W/C Ratio	Slump (in)	Air (%)	Specimen ID	F/T Durability (%)
Water	544	20.1	3	0.455	0.75	7.00	1RJ5B125	76.7
Reducer		Note that the second of the second					1RJ5B126	81.8
Interval 3			NO	T INCLUDE		************************	1RJ5B127	65.3
				.,			1RJ5B128	51.2
							1RJ5B129	83
		N MAT MALE AND A SECOND ASSECTION ASS					1RJ5B130	79.3
			y				1RJ5B131	80.8
							1RJ5B132	79.7
		-					Average	80.2

Mix Name	Cement & FlyAsh (lb/yd^3)	WR (oz/yd^3)	Air Agent (oz/yd^3)	W/C Ratio	Slump (in)	Air (%)	Specimen ID	F/T Durability (%)
Water	548	19.8	3	0.445	1.25	6.10	1RJ5B149	77.7
Reducer		1			to at lices to temperature and the second of	The first of the second shorter an expense of the second state of	1RJ5B150	87.3
Interval 4	control of the second s				ter i de te i di anti-anti-anti-anti-anti-anti-anti-anti-		1RJ5B151	82.5
					The second section of the second section is a second		1RJ5B152	86.6
					Self-consistence (en en e	enderson on a sur	1RJ5B153	80.7
	NOTE: NOT THE REAL PROPERTY.	afaste a un ancimiento secono eccesi		the trace of the t			1RJ5B154	83.9
							1RJ5B155 1RJ5B156	82.2 88.4
							Average	84.1

APPENDIX B

(Air Void Analysis Worksheets)

Summary of speciman 1R021.CHO on 12/04/2001 ASTM C-457 Procedure A

Length = 106.193

Percent Air = 2.032

Average Air Void = 0.01226

Void/Paste Ratio = 0.039

Percent Paste = 51.51

Paste/Void Ratio = 25.35

Standard Dev of Air Void Sizes = 0.0295

Spacing Factor = 0.02911

97.73

Voids Per Inch = 1.66 Specific Surface = 326.28

Specification Range: 0.004 - 0.008

Specification Range: 600 - 1100

	Frequency Distribution of Air Voids (in Distance Pulse Counts)										
Lower	Upper	No.	Pct.	Lower	Upper	No.	Pct.	Lower	Upper	No.	Pct.
0	49 =	7	3.98	50	99 =	33	22.73	100	149 =	13	30.11
150	199 =	11	36.36	200	249 =	4	38.64	250	299 =	10	44.32
300	349 =	8	48.86	350	399 =	4	51.14	400	449 =	4	53.41
450	499 =	7	57.39	500	549 =	2	58.52	550	599 =	1	59.09
600	649 =	4	61.36	650	699 =	2	62.5	700	749 =	5	65.34
750	799 =	6	68.75	800	849 =	2	69.89	850	899 =	5	72.73
900	949 =	2	73.86	950	999 =	4	76.14	1000	1049 =	2	77.27
1050	1099 =	2	78.41	1100	1149 =	2	79.55	1150	1199 =	2	80.68
1200	1249 =	2	81.82	1250	1299 =	2	82.95	1300	1349 =	1	83.52
1350	1399 =	2	84.66	1400	149 =	1	85.23	1450	1499 =	0	85.23
1500	1549 =	1	85.8	1550	1599 =	0	85.8	1600	1649 =	1	86.36
1650	1699 =	0	86.36	1700	1749 =	0	86.36	1750	1499 =	0	86.36
1800	1849 =	1	86.93	1850	1899 =	1	87.5	1900	1949 =	0	87.5
1950	1999 =	1	88.07	2000	2499 =	1	88.64	2500	2999 =	2	89.77
3000	3499 =	2	90.91	3500	3999 =	4	93.18	4000	4499 =	2	94.32
4500	4999 =	1	94.89	5000	5499 =	1	95.45	5500	5999 =	1	96.02
6000	6499 =	0	96.02	6500	6999 =	1	96.59	7000	7499 =	1	97.16

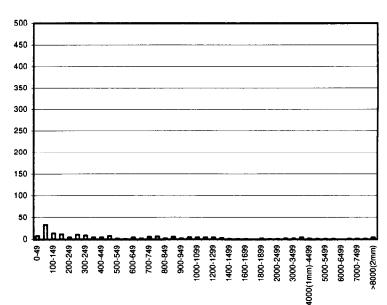
= 0008

Percent Air Summary by Size

7999 =

7500

Size	Concrete	Mortar
Total	2.032	3.944
<600	0.193	0.375
Tot Pct	59.09	
Tot No	104	
600-4000 (1 mm)	0.758	1.471
Tot Pct	34.09	
Tot No	60	
4000 (1 mm) - 8000 (2mm)	0.431	0.837
Tot Pct	4.55	
Tot No	8	
> 8000 (2mm)	0.65	1.261
Tot Pct	0	
Tot No	4	



100

Summary of speciman 1R087.CHO on 12/04/2001 ASTM C-457 Procedure A

Length = 94.28951

Percent Air = 3.726

Average Air Void = 0.00367

Void/Paste Ratio = 0.079

Percent Paste = 46.95

Paste/Void Ratio = 12.6

Standard Dev of Air Void Sizes = 0.00873

Voids Per Inch = 10.16

Spacing Factor = 0.00644

Specific Surface = 1090.66

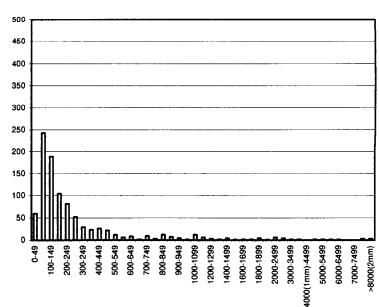
Specification Range: 0.004 - 0.008

Specification Range: 600 - 1100

<u>Frequ</u>	<u>ency Di</u>	stributior	<u>1 OT AIR VO</u>	<u>ias (in D</u>	<u>istance</u>	Puise Co	<u>unts)</u>
NI.	D-4	1	Hanas	81-	D-4	1	11

Lower	Upper	No.	Pct.	Lower	Upper	No.	Pct.	Lower	Upper	No.	Pct.
0	49 =	59	6.16	50	99 =	243	31.52	100	149 =	189	51.25
150	199 =	104	62.11	200	249 =	81	70.56	250	299 =	52	75.99
300	349 =	30	79.12	350	399 =	24	81.63	400	449 =	27	84.45
450	499 =	22	86.74	500	549 =	12	88	550	599 =	6	88.62
600	649 =	8	89.46	650	699 =	2	89.67	700	749 =	9	90.61
750	799 =	3	90.92	800	849 =	12	92.17	850	899 =	7	92.9
900	949 =	4	93.32	950	999 =	1	93.42	1000	1049 =	7	94.15
1050	1099 =	5	94.68	1100	1149 =	4	95.09	1150	1199 =	2	95.3
1200	1249 =	0	95.3	1250	1299 =	3	95.62	1300	1349 =	1	95.72
1350	1399 =	1	95.82	1400	149 =	2	96.03	1450	1499 =	2	96.24
1500	1549 =	1	96.35	1550	1599 =	0	96.35	1600	1649 =	1	96.45
1650	1699 =	1	96.56	1700	1749 =	0	96.56	1750	1499 =	2	96.76
1800	1849 =	3	97.08	1850	1899 =	1	97.18	1900	1949 =	0	97.18
1950	1999 =	1	97.29	2000	2499 =	6	97.91	2500	2999 =	4	98.33
3000	3499 =	2	98.54	3500	3999 =	2	98.75	4000	4499 =	0	98.75
4500	4999 =	2	98.96	5000	5499 =	2	99.16	5500	5999 =	1	99.27
6000	6499 =	1	99.37	6500	6999 =	0	99.37	7000	7499 =	0	99.37
7500	7999 =	3	99.69	>=	8000 =	3	100				

Size	Concrete	Mortar
Total	3.726	7.936
<600	1.53	3.259
Tot Pct	88.62	
Tot No	849	
600-4000 (1 mm)	1.32	2.811
Tot Pct	10.13	
Tot No	97	
4000 (1 mm) - 8000 (2mm)	0.579	1.233
Tot Pct	0.94	
Tot No	9	
> 8000 (2mm)	0.298	0.634
Tot Pct	0	
Tot No	3	



Summary of speciman 1R111.CHO on 12/04/2001 ASTM C-457 Procedure A

Length = 93.72668

Percent Air = 4.876

Average Air Void = 0.00346

Void/Paste Ratio = 0.095

Percent Paste = 51.29

Paste/Void Ratio = 10.52

Standard Dev of Air Void Sizes = 0.00741

Voids Per Inch = 14.07

Spacing Factor = 0.00562

Specific Surface = 1154.51

Specification Range: 0.004 - 0.008

Specification Range: 600 - 1100

Frequency Distribution of Air Voids (in Distance Pulse Counts)											
Lower	Upper	No.	Pct.	Lower	Upper	No.	Pct.	Lower	Upper	No.	Pct.
0	49 =	59	4.47	50	99 =	335	29.87	100	149 =	286	51.55
150	199 =	132	61.56	200	249 =	97	68.92	250	299 =	73	74.45
300	349 =	40	77.48	350	399 =	52	81.43	400	449 =	27	83.47
450	499 =	24	85.29	500	549 =	20	86.81	550	599 =	17	88.1
600	649 =	16	89.31	650	699 =	8	89.92	700	749 =	11	90.75
750	799 =	10	91.51	800	849 =	8	92.12	850	899 =	6	92.57
900	949 =	6	93.03	950	999 =	6	93.48	1000	1049 =	6	93.93
1050	1099 =	6	94.39	1100	1149 =	2	94.54	1150	1199 =	6	95
1200	1249 =	4	95.3	1250	1299 =	5	95.68	1300	1349 =	4	95.98
1350	1399 =	3	96.21	1400	149 =	0	96.21	1450	1499 =	2	96.36
1500	1549 =	3	96.59	1550	1599 =	2	96.74	1600	1649 =	4	97.04
1650	1699 =	2	97.19	1700	1749 =	1	97.27	1750	1499 =	1	97.35
1800	1849 =	1	97.42	1850	1899 =	4	97.73	1900	1949 =	1	97.8
1950	1999 =	2	97.95	2000	2499 =	6	98.41	2500	2999 =	2	98.56
3000	3499 =	4	98.86	3500	3999 =	4	99.17	4000	4499 =	2	99.32
4500	4999 =	0	99.32	5000	5499 =	3	99.55	5500	5999 =	1	99.62
6000	6499 =	2	99.77	6500	6999 =	0	99.77	7000	7499 =	1	99.85
7500	7999 =	0	99.85	>=	= 0008	2	100				

Size	Concrete	Mortar	
Total	4.876	9.507	500
<600	2.174	4.238	450
Tot Pct	88.1		400
Tot No	1162		
600-4000 (1 mm)	1.933	3.769	350
Tot Pct	11.07		300
Tot No	146		250
4000 (1 mm) - 8000 (2mm)	0.53	1.034	
Tot Pct	0.68		200
Tot No	9		150
> 8000 (2mm)	0.239	0.466	100
Tot Pct	0		
Tot No	2		50 11 11 11 11 11 11 11 11 11 11 11 11 11
			0
			0-49 0-49 1-48 1-48 1-48 1-549
			0-49 100-149 200-249 300-249 400-449 500-649 700-749 800-849 1200-1699 1200-1699 1800-1699 1800-1699 1800-1699 1800-1699 1800-1699 1800-1699 1800-1699 1800-1699
			008 008 008 008 008 008 008 008 008 008
			0-49 100-149 200-249 300-249 400-449 500-549 600-649 1000-1099 1200-1299 1400-1499 1600-1699 1600-1699 2000-2499 3000-5499 5000-5499 5000-5499 5000-5499

Summary of speciman 1R183.CHO on 12/04/2001 ASTM C-457 Procedure A

Length = 93.95881

Percent Air = 4.332

Average Air Void = 0.00324

Void/Paste Ratio = 0.088

Percent Paste = 49.41

Paste/Void Ratio = 11.41

Standard Dev of Air Void Sizes = 0.00795

Voids Per Inch = 13.39

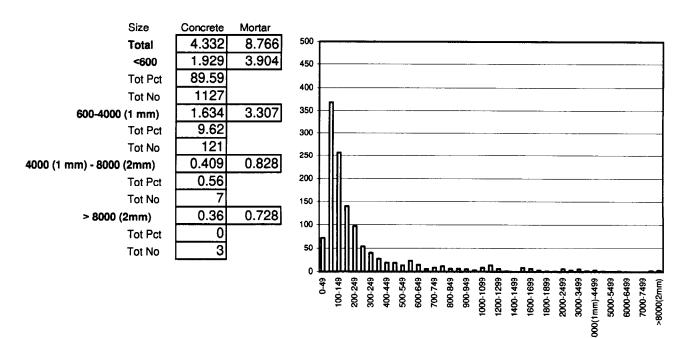
Spacing Factor = 0.00544

Specific Surface = 1236.38

Specification Range: 0.004 - 0.008

Specification Range: 600 - 1100

Frequency Distribution of Air Voids (in Distance Pulse Counts)											
Lower	Upper	No.	Pct.	Lower	Upper	No.	Pct.	Lower	Upper	No.	Pct.
0	49 =	72	5.72	50	99 =	368	34.98	100	149 =	257	55.41
150	199 =	140	66.53	200	249 =	97	74.24	250	299 =	54	78.54
300	349 =	39	81.64	350	399 =	27	83.78	400	449 =	19	85.29
450	499 =	18	86.72	500	549 =	13	87.76	550	599 =	23	89.59
600	649 =	14	90.7	650	699 =	5	91.1	700	749 =	8	91.73
750	799 =	11	92.61	800	849 =	6	93.08	850	899 =	6	93.56
900	949 =	5	93.96	950	999 =	3	94.2	1000	1049 =	4	94.52
1050	1099 =	4	94.83	1100	1149 =	5	95.23	1150	1199 =	8	95.87
1200	1249 =	5	96.26	1250	1299 =	1	96.34	1300	1349 =	0	96.34
1350	1399 =	1	96.42	1400	149 =	0	96.42	1450	1499 =	0	96.42
1500	1549 =	2	96.58	1550	1599 =	6	97.06	1600	1649 =	6	97.54
1650	1699 =	0	97.54	1700	1749 =	2	97.69	1750	1499 =	1	97.77
1800	1849 =	1	97.85	1850	1899 =	0	97.85	1900	1949 =	0	97.85
1950	1999 =	1	97.93	2000	2499 =	6	98.41	2500	2999 =	3	98.65
3000	3499 =	5	99.05	3500	3999 =	2	99.21	4000	4499 =	3	99.44
4500	4999 =	1	99.52	5000	5499 =	0	99.52	5500	5999 =	1	99.6
6000	6499 =	0	99.6	6500	6999 =	0	99.6	7000	7499 =	0	99.6
7500	7999 =	2	99.76	>=	= 0008	3	100				



Summary of speciman 1R043.CHO on 12/05/2001 ASTM C-457 Procedure A

Length = 94.48513

Percent Air = 5.975

Average Air Void = 0.0049

Void/Paste Ratio = 0.131

Percent Paste = 45.47

Paste/Void Ratio = 7.61

Standard Dev of Air Void Sizes = 0.01293

Voids Per Inch = 12.19

Spacing Factor = 0.00687

Specific Surface = 816.21

Specification Range: 0.004 - 0.008

Specification Range: 600 - 1100

Frequency Distribution of Air Voids (in Distance Pulse Counts)											
Lower	Upper	No.	Pct.	Lower	Upper	No.	Pct.	Lower	Upper	No.	Pct.
0	49 =	27	2.34	50	99 =	183	18.23	100	149 =	192	34.9
150	199 =	115	44.88	200	249 =	103	53.82	250	299 =	83	61.02
300	349 =	52	65.54	350	399 =	45	69.44	400	449 =	40	72.92
450	499 =	36	76.04	500	549 =	29	78.56	550	599 =	18	80.12
600	649 =	23	82.12	650	699 =	15	83.42	700	749 =	17	84.9
750	799 =	12	85.94	800	849 =	14	87.15	850	899 =	7	87.76
900	949 =	5	88.19	950	999 =	9	88.98	1000	1049 =	7	89.58
1050	1099 =	8	90.28	1100	1149 =	7	90.89	1150	1199 =	11	91.84
1200	1249 =	2	92.01	1250	1299 =	5	92.45	1300	1349 =	9	93.23
1350	1399 =	12	94.27	1400	149 =	1	94.36	1450	1499 =	5	94.79
1500	1549 =	2	94.97	1550	1599 =	3	95.23	1600	1649 =	4	95.57
1650	1699 =	4	95.92	1700	1749 =	1	96.01	1750	1499 =	2	96.18
1800	1849 =	1	96.27	1850	1899 =	1	96.35	1900	1949 =	2	96.53
1950	1999 =	1	96.61	2000	2499 =	11	97.57	2500	2999 =	8	98.26
3000	3499 =	9	99.05	3500	3999 =	3	99.31	4000	4499 =	1	99.39
4500	4999 =	0	99.39	5000	5499 =	0	99.39	5500	5999 =	2	99.57
6000	6499 =	1	99.65	6500	6999 =	1	99.74	7000	7499 =	0	99.74
7500	7999 =	0	99.74	>=	8000 =	3	100				

	_		
Size	Concrete	Mortar	
Total	5.975	13.141	500
<600	2.085	4.586	450
Tot Pct	80.12		400
Tot No	923		400
600-4000 (1 mm)	2.996	6.59	350
Tot Pct	19.18		300
Tot No	221		250
4000 (1 mm) - 8000 (2mm)	0.299	0.657	
Tot Pct	0.43		200
Tot No	5		150
> 8000 (2mm)	0.595	1.308	100
Tot Pct	0]
Tot No	3		50 _
			0 NIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII
			0-49 1-149 1-249 1-549 1-549 1-549 1-549 1-549 1-549 1-549 1-649 1
			0-49 100-149 300-249 300-249 300-649 500-649 900-1099 900-1099 900-1099 900-1099 900-1099 900-3499 900-3499 900-3499 900-3499
			0-49 100-149 200-249 300-249 400-449 500-649 700-749 1000-1099 1200-1299 1400-1499 1600-1699 1600-1499 1600-1499 1600-1499 1600-1499 1600-1499 1600-1499 1600-1499 1600-1499 1600-1499 1600-1499 1600-1499 1600-1499 1600-1499 1600-1499 1600-1499
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Summary of speciman 1R065.CHO on 12/05/2001 ASTM C-457 Procedure A

Length = 94.63906

Percent Air = 4.025

Average Air Void = 0.00445

Void/Paste Ratio = 0.084

Percent Paste = 48.13

Paste/Void Ratio = 11.96

Standard Dev of Air Void Sizes = 0.0095

Voids Per Inch = 9.04

Spacing Factor = 0.00764

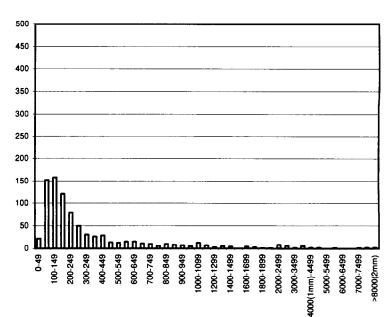
Specific Surface = 898.78

Specification Range: 0.004 - 0.008

Specification Range: 600 - 1100

Frequency Distribution of Air Voids (in Distance Pulse Counts)											
Lower	Upper	No.	Pct.	Lower	Upper	No.	Pct.	Lower	Upper	No.	Pct.
0	49 =	22	2.57	50	99 =	152	20.33	100	149 =	158	38.79
150	199 =	121	52.92	200	249 =	80	62.27	250	299 =	50	68.11
300	349 =	31	71.73	350	399 =	27	74.88	400	449 =	29	78.27
450	499 =	14	79.91	500	549 =	13	81.43	550	599 =	15	83.18
600	649 =	15	84.93	650	699 =	11	86.21	700	749 =	10	87.38
750	799 =	5	87.97	800	849 =	10	89.14	850	899 =	8	90.07
900	949 =	7	90.89	950	999 =	5	91.47	1000	1049 =	6	92.17
1050	1099 =	7	92.99	1100	1149 =	4	93.46	1150	1199 =	3	93.81
1200	1249 =	2	94.04	1250	1299 =	1	94.16	1300	1349 =	1	94.28
1350	1399 =	4	94.74	1400	149 =	1	94.86	1450	1499 =	3	95.21
1500	1549 =	0	95.21	1550	1599 =	0	95.21	1600	1649 =	2	95.44
1650	1699 =	2	95.68	1700	1749 =	0	95.68	1750	1499 =	3	96.03
1800	1849 =	1	96.14	1850	1899 =	0	96.14	1900	1949 =	1	96.26
1950	1999 =	0	96.26	2000	2499 =	8	97.2	2500	2999 =	6	97.9
3000	3499 =	2	98.13	3500	3999 =	6	98.83	4000	4499 =	2	99.07
4500	4999 =	2	99.3	5000	5499 =	0	99.3	5500	5999 =	1	99.42
6000	6499 =	0	99.42	6500	6999 =	0	99.42	7000	7499 =	1	99.53
7500	7999 =	2	99 77	>=	8000 =	2	100				

Size	Concrete	Mortar
Total	4.025	8.364
<600	1.463	3.04
Tot Pct	83.18	
Tot No	712	
600-4000 (1 mm)	1.82	3.782
Tot Pct	15.65	
Tot No	134	
4000 (1 mm) - 8000 (2mm)	0.49	1.019
Tot Pct	0.93	
Tot No	8	
> 8000 (2mm)	0.251	0.522
Tot Pct	0	
Tot No	2	



Summary of speciman 1R135.CHO on 12/05/2001 ASTM C-457 Procedure A

Length = 94.0634

Percent Air = 3.901

Average Air Void = 0.00477

Void/Paste Ratio = 0.08

Percent Paste = 48.64

Paste/Void Ratio = 12.47

Standard Dev of Air Void Sizes = 0.00887

Spacing Factor = 0.00834

Voids Per Inch = 8.18 Specific Surface = 838.17

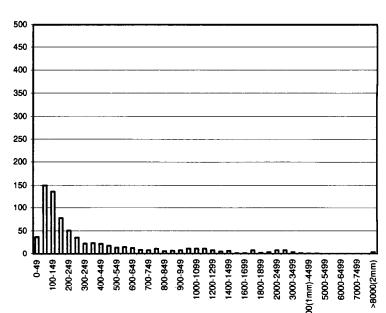
Specification Range: 0.004 - 0.008

Specification Range: 600 - 1100

Frequency Distribution of Air Voids (in Distance Pulse Counts)

Lower	Upper	No.	Pct.	Lower	Upper	No.	Pct.	Lower	Upper	No.	Pct.
0	49 =	37	4.81	50	99 =	150	24.32	100	149 =	135	41.87
150	199 =	79	52.15	200	249 =	51	58.78	250	299 =	36	63.46
300	349 =	23	66.45	350	399 =	24	69.57	400	449 =	22	72.43
450	499 =	18	74.77	500	549 =	14	76.59	550	599 =	15	78.54
600	649 =	13	80.23	650	699 =	9	81.4	700	749 =	8	82.44
750	799 =	11	83.88	800	849 =	6	84.66	850	899 =	7	85.57
900	949 =	8	86.61	950	999 =	12	88.17	1000	1049 =	9	89.34
1050	1099 =	3	89.73	1100	1149 =	7	90.64	1150	1199 =	5	91.29
1200	1249 =	2	91.55	1250	1299 =	6	92.33	1300	1349 =	3	92.72
1350	1399 =	2	92.98	1400	149 =	6	93.76	1450	1499 =	1	93.89
1500	1549 =	2	94.15	1550	1599 =	0	94.15	1600	1649 =	2	94.41
1650	1699 =	0	94.41	1700	1749 =	1	94.54	1750	1499 =	7	95.45
1800	1849 =	2	95.71	1850	1899 =	1	95.84	1900	1949 =	2	96.1
1950	1999 =	2	96.36	2000	2499 =	8	97.4	2500	2999 =	8	98.44
3000	3499 =	4	98.96	3500	3999 =	2	99.22	4000	4499 =	1	99.35
4500	4999 =	1	99.48	5000	5499 =	0	99.48	5500	5999 =	0	99.48
6000	6499 =	0	99.48	6500	6999 =	0	99.48	7000	7499 =	0	99.48
7500	7999 =	0	99.48	>=	8000 =	4	100				

Size	Concrete	Mortar
Total	3.901	8.021
. <600	1.213	2.494
Tot Pct	78.54	
Tot No	604	
600-4000 (1 mm)	2.193	4.508
Tot Pct	20.68	
Tot No	159	
4000 (1 mm) - 8000 (2mm)	0.095	0.196
Tot Pct	0.26	
Tot No	2	
> 8000 (2mm)	0.4	0.823
Tot Pct	0	
Tot No	4	



Summary of speciman 1R159.CHO on 12/05/2001 ASTM C-457 Procedure A

Length = 94.15021

Percent Air = 3.617

Average Air Void = 0.00429

Void/Paste Ratio = 0.071

Percent Paste = 50.85

Paste/Void Ratio = 14.06

Standard Dev of Air Void Sizes = 0.01333

Voids Per Inch = 8.43

Spacing Factor = 0.0079

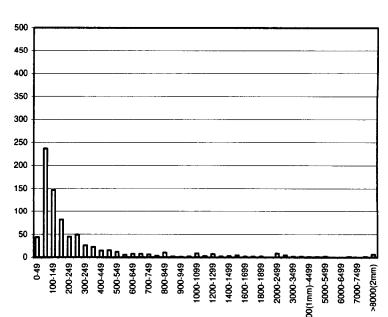
Specific Surface = 932.72

Specification Range: 0.004 - 0.008

Specification Range: 600 - 1100

		Freque	ency Dis	stribution	of Air Voic	is (in Di	stance I	Pulse Co	<u>unts)</u>		
Lower	Upper	No.	Pct.	Lower	Upper	No.	Pct.	Lower	Upper	No.	Pct.
0	49 =	44	5.54	50	99 =	236	35.26	100	149 =	147	53.78
150	199 =	82	64.11	200	249 =	45	69.77	250	299 =	49	75.94
300	349 =	25	79.09	350	399 =	22	81.86	400	449 =	14	83.63
450	499 =	15	85.52	500	549 =	11	86.9	550	599 =	5	87.53
600	649 =	7	88.41	650	699 =	7	89.29	700	749 =	6	90.05
750	799 =	3	90.43	800	849 =	10	91.69	850	899 =	2	91.94
900	949 =	1	92.07	950	999 =	2	92.32	1000	1049 =	3	92.7
1050	1099 =	5	93.32	1100	1149 =	1	93.45	1150	1199 =	2	93.7
1200	1249 =	5	94.33	1250	1299 =	2	94.58	1300	1349 =	0	94.58
1350	1399 =	2	94.84	1400	149 =	2	95.09	1450	1499 =	1	95.21
1500	1549 =	1	95.34	1550	1599 =	3	95.72	1600	1649 =	2	95.97
1650	1699 =	0	95.97	1700	1749 =	1	96.1	1750	1499 =	1	96.22
1800	1849 =	2	96.47	1850	1899 =	0	96.47	1900	1949 =	0	96.47
1950	1999 =	0	96.47	2000	2499 =	8	97.48	2500	2999 =	4	97.98
3000	3499 =	2	98.24	3500	3999 =	2	98.49	4000	4499 =	1	98.61
4500	4999 =	1	98.74	5000	5499 =	2	98.99	5500	5999 =	0	98.99
6000	6499 =	0	98.99	6500	6999 =	1	99.12	7000	7499 =	0	99.12
7500	7999 =	1	99.24	>=	= 0008	6	100				

	Size	Concrete	Mortar
	Total	3.617	7.113
	<600	1.2	2.36
	Tot Pct	87.53	
	Tot No	695	
600-4000 ((1 mm)	1.238	2.435
	Tot Pct	10.96	
	Tot No	87	
4000 (1 mm) - 8000 (2mm)	0.358	0.704
	Tot Pct	0.76	
	Tot No	6	
> 8000 (2	mm)	0.821	1.614
	Tot Pct	0	
	Tot No	6	



APPENDIX C

(Chloride Permeability Testing)

CONTROL MIXES

	Cement &		Chloride Permeability							
Mix Name	FlyAsh (lb/yd^3)	WR (oz/yd^3)	Air Agent (oz/yd^3)	W/C Ratio	Siump (in)	Air (%)	Specimen ID	28-Day Lift 1	28-Day Lift 2	56-Day Lift 3
Control Mix Interval 1	573	0.0	8.0	0.455 RESULTS	1.50 NOT INCLL	1.50 J DE D	1R089 1R090	4503	4451	2955 3552

	Cement &			,			Chloride Permeability				
Mix Name	RyAsh (lb/yd^3)	WR (oz/yd^3)	Air Agent (oz/yd^3)	W/C Ratio	Slump (in)	Air (%)	Specimen ID	28-Day Lift 1	28-Day Lift 2	56-Day Lift 3	
Control Mix	573	0.0	8.0	0.455	1.50	6.90	1F085	4557	4215	3949	
interval 2		***************************************					1R086	4834	5029	3886	
					-		AVG.	4696	4622	3918	

	Cement &							Chloride Pe	rmeability	
Mix Name	FlyAsh (lb/yd^3)	WR (oz/yd^3)	Air Agent (oz/yd^3)	W/C Ratio	Slump (in)	Air (%)	Specimen ID	28-Day Lift 1	28-Day Lift 2	56-Day Lift 3
Control Mix	573	0.0	9.0	0.457	1.75	6.70	1R109	4500	6267	4327
Interval 3				************	p. 100 (2 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 +		1R110	3841	4862	3511
							AVG.	4171	5565	3919

	Cement &				Chloride Pe	rmeability	56-Day			
Mix Name	FlyAsh (lb/yd^3)	WR (oz/yd^3)	Air Agent (oz/yd^3)	WC Patio	Slump (in)	Air (%)	Specimen ID	28-Day Lift 1	28-Day Lift 2	•
Control Mix	573	0.0	9.0	0.457	2.25	6.90	1R181	6080	5892	4766
Interval 4	and the second second second second	ender i it is service anno e i anno e i	y i i i ini ni namatana na arawa a na na na na	and remain to the second resolution to			1R182	5835	6320	3822
							AVG.	5958	6106	4294

High	4,000	High wic ratio (≕>∪.6)
Moderate	2,000-4,000	Mod. w/c ratio (0.4-0.5)
Low	1,000-2,000	Low w/c ratio
Very Low	100-1,000	Latex Mod. Concrete
Nedicible	100	Polymer Impregnated

	28-DAY	28-DAY	56-DAY
	TOP	MDDLE	BOTTOM
	LIFT 1	UFT 2	LIFT 3
TOTAL AVG.	4941	5431	4044

WATER REDUCER MIXES

	Cement &							Chloride Pe	rmeability	
	FlyAsh	WR	Air Agent	W/C	Slump			28-Day	28-Day	56-Day
Mix Name	(lb/yd^3)	(oz/yd^3)	(oz/yd^3)	Ratio	(in)	Air (%)	Specimen ID	Lift 1	Lift 2	Lift 3
Water	546	20.0	2.5	0.467	1.00	8.00	1R041	3516	3431	4430
Reducer							1R042	3838	3708	4310
Interval 1						the control of the section to the	AVG.	3677	3570	4370
	Cement &							Chloride Pe	rmeability	
	FlyAsh	WR	Air Agent	W/C	Slump			28-Day	28-Day	56-Day
Mix Name	(lb/yd^3)	(oz/yd^3)	(oz/yd^3)	Ratio	(in)	Air (%)	Specimen ID	Lift 1	Lift 2	Lift 3
Water	546	20.0	2.5	0.467	1.50	5.80	1R063	3734	3776	2596
Reducer		or formanism or a second	ere e e e e e e e e e e e e e e e e e e			ere i e e e e e e escora esce	1R064	3428	3485	3305
Interval 2		and Sign and an in the grade and a second of the control of the co	saaran		oference or a second	and in the contract of the con	AVG.	3581	3631	2951
				i						
	Cement &						Chloride Permeability			
	FlyAsh	WR	Air Agent	W/C	Slump			28-Day	28-Day	56-Day
Mix Name	(lb/yd^3)	(oz/yd^3)	(oz/yd^3)	Ratio	(in)	Air (%)	Specimen ID	Lift 1	Lift 2	Lift 3
Water	546	20.0	3	0.448	0.75	7.00	1R133	3574	3621	3047
Reducer		o Barramanan in terresion and					1R134	3304	2989	2779
Interval 3							AVG.	3439	3305	2913
	Cement &							Chloride Pe	rmeability	
	FlyAsh	WR	Air Agent	W/C	Slump			28-Day	28-Day	56-Day
Mix Name	(lb/yd^3)	(oz/yd^3)	(oz/yd^3)	Ratio	(in)	Air (%)	Specimen ID	Lift 1	Lift 2	Lift 3
Water	546	20.0	3	0.448	1.25	6.10	1R157	3502	4208	3148
Reducer	manantin ne meren e e militar e e Meren in menteroni interiori della interiori	The state of the s	annotates an absent him of the above or the second		general en entre e i tre commence aceg	etalolotetet totala elevitat on erecension energiand	1R158	2952	3253	2692
Interval 4			and the second section of the second	TO THE RESIDENCE OF THE PERSON	### *** * * * * * * * * * * * * * * * *	alekside side on graden is to a new angles	AVG.	3227	3731	2920
High	4,000	High w/c ra	tio (=>0.6)							
Moderate	2,000-4,000	Mod. w/c ra	tio (0.4-0.5)					28-DAY	28-DAY	56-DAY
Low	1,000-2,000	Low w/c rat	io					TOP	MIDDLE	BOTTOM
Very Low	100-1,000	Latex Mod.	Concrete					LIFT 1	LIFT 2	LIFT 3

Negligible

100

Polymer Impregnated

TOTAL AVG.

3481

3559

3288

APPENDIX D

(Compressive and Flexural Strength Testing)

CONTROL MIX

Mix Name	Cement & FlyAsh (lb/yd^3)	WR (oz/yd^3)	Air Agent (oz/yd^3)	W/C Ratio	Slump (in)	Air (%)	7-Day Compress. Strength	28-Day Compress. Strength	7-Day Flexural Strength	28-Day Flexural Strength
Control Mix	<u>573</u>	<u>0.0</u>	<u>8.0</u>	0.412	1.50	1.50	4761	6381	614	872
Interval 1							4885	6250	668	784
							4809	6535	633	771
				Standard	Average Deviation		4818 63	6389 143	638 27	809 55

Mix Name	Cement & FlyAsh (lb/yd^3)	WR (oz/yd^3)	Air Agent (oz/yd^3)	W/C Ratio	Slump (in)	Air (%)	7-Day Compress. Strength	28-Day Compress. Strength	7-Day Flexural Strength	28-Day Flexural Strength
Control Mix	580	0.0	8.0	0.457	1.50	6.90	4064	5547	652	695
Interval 2							3992	5270	462	678
							3554	5157	537	661
					Average		3870	5325	550	678
				Standard	Deviation		276	201	96	17

Mix Name	Cement & FlyAsh (lb/yd^3)	WR (oz/yd^3)	Air Agent (oz/yd^3)	W/C Ratio	Slump (in)	Air (%)	7-Day Compress. Strength	28-Day Compress. Strength	7-Day Flexural Strength	28-Day Flexural Strength
Control Mix	<u>573</u>	0.0	<i>8.0</i>	0.412	1.75	6.70	3574	4403	533	737
Interval 3	Commence of the control of the contr		error per fortester and code.	to the district of the first of the dispersion of the			3376	4441	557	626
,			**	control of the contro			3368	4870	561	631
			Making to statement their total to select	Standard	Average Deviation		3439 117	4571 259	550 15	665 63

Mix Name	Cement & FlyAsh (lb/yd^3)	WR (oz/yd^3)	Air Agent (oz/yd^3)	W/C Ratio	Slump (in)	Air (%)	7-Day Compress. Strength	28-Day Compress. Strength	7-Day Flexural Strength	28-Day Flexural Strength
Control Mix	570	0.0	9.0	0.453	2.25	6.90	3594	4599	528	654
Interval 4							3455	4404	508	599
		The file of the second	e mente comme consequences e accident				3507	4464	524	643
					Average		3519	4489	520	632
				Standard	Deviation		70	100	11	29

WR MIXES

Mix Name	Cement & FlyAsh (lb/yd^3)	WR (oz/yd^3)	Air Agent (oz/yd^3)	W/C Ratio	Slump (in)	Air (%)	7-Day Compress. Strength	28-Day Compress. Strength	7-Day Flexural Strength	28-Day Flexural Strength
Water	<u>546</u>	<u> 20.0</u>	<u>2.5</u>	<u>0.428</u>	1.00	8.00	2736	4130	521	652
Reducer							3206	4049	503	615
Interval 1							3288	4519	518	710
	· · ·			·	Average		3077	4233	514	659
				Standard	Deviation		298	251	10	48

Mix Name	Cement & FlyAsh (lb/yd^3)	WR (oz/yd^3)	Air Agent (oz/yd^3)	W/C Ratio	Slump (in)	Air (%)	7-Day Compress. Strength	28-Day Compress. Strength	7-Day Flexural Strength	28-Day Flexural Strength
Water	544	19.8	2.4	0.368	1.50	5.80	4173	6310	607	712
Reducer					:		4405	6010	614	775
Interval 2							4155	5832	629	701
					Average	-	4244	6051	617	729
			An harmonic or an area and a second	Standard	Deviation		139	242	11	40

Mix Name	Cement & FlyAsh (lb/yd^3)	WR (oz/yd^3)	Air Agent (oz/yd^3)	W/C Ratio	Slump (in)	Air (%)	7-Day Compress. Strength	28-Day Compress. Strength	7-Day Flexural Strength	28-Day Flexural Strength
Water	544	20.1	3	0.455	0.75	7.00	4153	5619	584	730
Reducer			·	t titeline i no renochaniste	i se	protein note to we continue in the	4426	5546	548	698
Interval 3							4090	5574	559	758
					Average		4223	5580	564	729
			A-840 - 100 - 10 - 0000 - 0000 - 000	Standard	Deviation		179	37	18	30

	Cement &						7-Day	28-Day	7-Day	28-Day
New Maria	FlyAsh	WR	Air Agent	W/C	Slump	A:- /0/ \		Compress.	Flexural	Flexural
Mix Name	(lb/yd^3)	(oz/yd^3)	(oz/yd^3)	Ratio	(in)	Air (%)	Strength	Strength	Strength	Strength
Water	548	19.8	3	0.445	1.25	6.10	4708	5738	651	738
Reducer			:			reconstrumentary and the consum	4422	5611	639	752
Interval 4					TO THE REST OF THE PARTY OF THE		4486	5839	600	756
					Average		4539	5729	630	749
				Standard	Deviation		150	114	27	9